APPENDIX B

DERIVATIONS OF FORMULAS FOR ASSEMBLY INTERFERENCES

The interferences Δ_n calculated in the text are the interferences required on the component parts as manufactured. However, the manufactured interference is not equal to the interference as assembled. The multi-ring container is taken as an example. It is assumed the rings are shrink-fit assembled one-by-one from the inside. The outer rings expand as they are shrunk on and the assembly interference for the next ring to be fitted is increased beyond the manufactured interference. The assembly interference between cylinders n and n + 1 is denoted by δ_n . It has dimensions of inches.

For assembly of cylinder n + 1 onto the other cylinders, δ_n is expressed as

$$\frac{\delta_n}{r_n} = \frac{\Delta_n}{r_n} + \frac{u'_n(r_n)}{r_n}$$
(B. 1)

where

- $u'_n(r_n) = radial displacement at r_n of cylinder n due to residual pressure <math>q'_{n-1}$ at r_{n-1} .
 - $\begin{array}{l} q_{n-1}' = \mbox{ residual pressure at } r_{n-1} \mbox{ due to assembly of cylinder n of wall } \\ & \mbox{ ratio } k_n \mbox{ onto a compound cylinder of wall ratio } k_1 k_2 \hdots \hdots k_{n-1} \\ & \mbox{ with an interference } \delta_{n-1}. \end{array}$

 q_{n-1}^{\prime} is calculated as follows:

$$\frac{\delta_{n-1}}{r_{n-1}} = \frac{u_n(r_{n-1}) - u_{n-1}(r_{n-1})}{r_{n-1}}$$

Substitution for u_n and u_{n-1} from Equation (17a) gives

$$\frac{\delta_{n-1}}{r_{n-1}} = \frac{1}{E_n(k_n^{2}-1)} \left[(1-v) q'_{n-1} + (1+v) q'_{n-1} k_n^2 \right] \\ - \frac{1}{E_{n-1}(k_{n-1}^2 k_{n-2}^2 \dots k_1^2 - 1)} \left[-(1-v) q'_{n-1} k_{n-1}^2 k_{n-2}^2 \dots k_1^2 - (1+v) q'_{n-1} \right]$$

$$= \frac{q_{n-1}'}{E} \left[\frac{k_n^2 + 1}{k_n^2 - 1} + \frac{k_{n-1}^2 k_{n-2}^2 \dots k_1^2 + 1}{k_{n-1}^2 k_{n-2}^2 \dots k_1^2 - 1} \right]$$

where $E_n = E_{n-1} = E$ is assumed.

Hence,
$$q_{n-1}^{\prime} = E\left(\frac{\delta_{n-1}}{r_{n-1}}\right) \frac{\left(k_{n-1}^{2}\right)\left(k_{n-1}^{2}k_{n-2}^{2}\cdots k_{1}^{2}-1\right)}{2\left(k_{n-1}^{2}k_{n-2}^{2}\cdots k_{1}^{2}-1\right)}$$
 (B.2)

Since

$$\frac{u_n'(r_n)}{r_n} = \frac{2 q_{n-1}'}{E(k_n^2 - 1)}$$
(B. 3)

Substitution of (B. 2) and (B. 3) into (B. 1) gives

$$\frac{\delta_{n}}{r_{n}} = \frac{\Delta_{n}}{r_{n}} + \frac{\delta_{n-1}}{r_{n-1}} \frac{\left(k_{n-1}^{2} k_{n-2}^{2} \dots k_{1}^{2} - 1\right)}{\left(k_{n}^{2} k_{n-1}^{2} k_{n-2}^{2} \dots k_{1}^{2} - 1\right)}$$
(B.4)

Now the $\frac{\delta_n}{r_n}$ can be calculated in sequence; i.e.,

$$\frac{\delta_1}{r_1} = \frac{\Delta_1}{r_1}$$

 $\frac{\delta_2}{r_2} = \frac{\Delta_2}{r_2} + \frac{\delta_1}{r_1} \frac{(k_1^2 - 1)}{(k_1^2 k_2^2 - 1)} , \text{ etc.}$

Equation (B. 4) applies if the rings are assembled from the inside out. If the rings are assembled one by one from the outside in, then the assembly interference for assembly of cylinder n-l into the other cylinders is

$$\frac{\delta_{n}}{r_{n}} = \frac{\Delta_{n}}{r_{n}} + \frac{\delta_{n+1}}{r_{n+1}} \frac{\left(k_{n}^{2}+1\right)}{2} \frac{\left(k_{n+1}^{2} k_{n+2}^{2} \cdots k_{N}^{2}-1\right)}{\left(k_{n}^{2} k_{n+1}^{2} \cdots k_{N}^{2}-1\right)}$$
(B.5)

Equation (B. 5) was found by an analogous procedure to that used in deriving (B. 4).

The method used to determine assembly interferences δ_n for the multi-ring container can also be used to determine assembly interferences for the other container designs. It is important to determine assembly interferences because they are larger than the manufactured interferences and excessive interference requirements may make a design impracticable.